

# Qualitative and Quantitative Evaluation of Permeability Changes during EOR Polymer Flooding Using Micromodels

Lucas Oliver Knobloch, Rafael Eduardo Hincapie Reina, Hendrik Födisch, Leonhard Ganzer

Institute of Petroleum Engineering, Clausthal University of Technology, Clausthal-Zellerfeld, Germany

Email: lucasknobloch@yahoo.de

**How to cite this paper:** Knobloch, L.O., Hincapie Reina, R.E., Foedisch, H. and Ganzer, L. (2018) Qualitative and Quantitative Evaluation of Permeability Changes during EOR Polymer Flooding Using Micromodels. *World Journal of Engineering and Technology*, 6, 332-349.

<https://doi.org/10.4236/wjet.2018.62021>

**Received:** January 27, 2018

**Accepted:** May 12, 2018

**Published:** May 15, 2018

Copyright © 2018 by authors and Scientific Research Publishing Inc.  
This work is licensed under the Creative Commons Attribution International License (CC BY 4.0).

<http://creativecommons.org/licenses/by/4.0/>



Open Access

## Abstract

Polymer solutions are used in chemical EOR processes to achieve incremental oil recoveries through obtaining favorable mobility ratios. In the process, the *in-situ* viscosity is a key parameter for the polymer flood design, as well as the changes in permeability due to the retention or adsorption (e.g.: plugging). Understanding the major causes of the plugging effects allows predicting injectivity problems as well as optimizing project design. The objective of this work is to use glass-silicon-glass micromodels in combination with tracer particles—attached to the flooded fluids—to qualitatively and quantitatively describe the extent of permeability changes after polymer injection. Laboratory work is performed in order to determine the physical properties of the polymer solutions when they flow through porous media, such as the presence of permeability reduction/plugging of the micromodel. A statistical analysis of the distribution and extent of plugged areas is performed and a study of the pressure response during various injection stages will complement the study. A biopolymer (Scleroglucan) was tested and compared to a commonly used polymer, giving a direct insight into their pros and cons. Five different concentrations of polymers were tested and put into relation with their quantitative and qualitative amount of sort of called retention. The amount of adsorption was determined experimentally in one case in order to draw the significance. By exploiting the potential of GSG-micromodels in combination with tracer particles, it was possible to visualize the reduction of flow paths and its increase during various injections for the first time. Expanding the working principle proposed in this work could provide further understanding of the behavior of any polymers. The results obtained and workflow presented in this work allow for additional understanding of polymer solutions behavior in flooding applications. Furthermore, the definition of optimized workflows to assess any kind of solutions in porous media and permeability changes is supported.

---

## Keywords

Enhanced Oil Recovery, Polymer Flooding, Micromodels, Retention, Plugging, Adsorption, Biopolymer

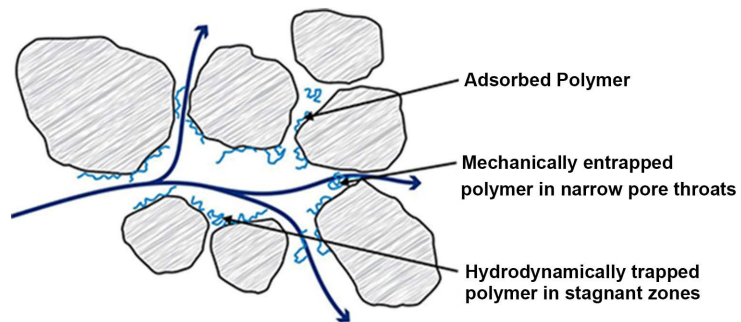
---

## 1. Introduction

The recovery of oil can be split into three phases, namely the primary recovery, secondary recovery and tertiary recovery. With the first two, only up to 40% of the OIIP can be produced. As oil is a limited resource, the importance of depletion of reservoirs has been increasing and will continue to do so. Thus, the tertiary recovery—also called improved oil recovery (IOR)—and its subpart the enhanced oil recovery (EOR) [1] are of significant importance. One key mechanism in EOR is polymer flooding, in which polymer is injected into the wellbore to increase oil mobility ratio and avoid viscous fingering of water [2] [3].

A very important aspect for the efficiency of a polymer is its viscosity under a specific in-situ shear rate. Viscosity can be understood as the resistance of a fluid to flow and it determines how well suited a polymer is to produce oil [4]. The downside with increasing viscosity is injectivity problems and higher chances of retention and therefore at some point plugging of the formation increase as well [5] [6].

The reduction in permeability during a polymer flood is due to several interactions of the fluid and the porous medium. Permeability reduction has a critical effect on flood productivity, especially in originally low permeable reservoirs. This reduction always leads to, in some extent, irreparable damage to the reservoir, a decrease in production efficiency and higher costs. The contributors to permeability reduction can be seen in **Figure 1**, namely adsorption, mechanical entrapment and hydrodynamic retention; the latter is almost negligible at low injection rates [2] [7] [8] [9]. Adsorption describes the bonding at contact of a polymer to the rock surface via van der Waal's and hydrogen bonding and increases with increasing rock surface. It is the only effect that removes polymer from a free powder/bulk solution. Polymers with a high molecular weight have shown high adsorption levels, which are accounted for by a layer thickness increase [2]. Furthermore, adsorption depends on the concentration of the used polymer solution. This can be explained with the increasing amount of polymer structures (chains) inside the solution [10]. Both, mechanical entrapment and hydrodynamic retention only occur during a flow through porous media. Mechanical entrapment refers to the molecules of the polymer being filtered out in narrow pore throats and in extreme cases building up and blocking passages, leading to a change of direction of the fluid flow. This mechanism occurs when the polymer fluid was not filtered accordingly to fit through the pore size of the porous medium. As to the nature of filtration, the most retention due to



**Figure 1.** Polymer retention mechanisms [8].

entrapment will occur near to the injection point and will decrease the further the fluid flows into the porous medium. Hydrodynamic retention means, that at high flow rates molecules of the polymer could get pushed into a cavity where there is no flow possible. The stream passing by that cavity prevents the molecules to reenter the stream due to hydrodynamic drag forces. This retention mechanism has been experienced to be to some extent reversible by stopping the flow for a short period of time. The drag forces vanish and the molecules are able to reenter the flow [2].

Due to the fact, that most oil reservoirs have a permeability of below 1 D, the experiments will focus on how the tested polymers will perform under realistic conditions. In EOR, it is important to design the fluids in a way so that they match the conditions of the reservoir in all aspects for the production to be feasible. Choosing an unsuited polymer fluid will lead to plugging and a loss in productivity. With the help of Glass-Silicon-Glass (GSG) micromodels we can track the polymers path through a simulated reservoir and can observe the several plugging mechanisms which occur during a polymer flood. These experiments are conducted with both Biopolymer (Scleroglucan) and the HPAM polymer (Flopaam) using different concentrations. Thus, we can compare their performances directly and give more insight into creating the best possible fluid solution.

The objective of this work is to experimentally and mathematically determine the influences of polymer flow in porous media; moreover, to present a comprehensive and systematic workflow to address and evaluate any kind of polymers. The flood experiments consist of porous media visualization in combination with differential pressure measurements at various stages of injection. These will be analyzed according to the following aspects:

- Comparison of the performance of a synthetic polymer with a biopolymer Scleroglucan.
- Occurrence and amount of plugging mechanisms, visible and not visible.
- Changes in permeability due to: 1) the retention mechanism of adsorption, 2) mechanical entrapment and 3) hydrodynamic retention.
- Polymer injectivity aspects such as: resistance factor (RF) and residual resistance factor (RRF).

## 2. Previously Reported Experiment Results Using Polymers

Manichand and Seright (2014) [9] reported that approximately half of Xanthan (Biopolymer) retention was due to adsorption and the other half to mechanical entrapment. Whereby, about 35.2% of the retention caused by HPAM was attributed to adsorption and the rest of 64.8% to mechanical entrapment [9].

A field test, Yariguí-Cantagallo Field in Columbia, over 24 months conducted with a HPAM resulted in a RRF of 3. With a resulting water cut of up to 5% the polymer flooding was considered both technically and economically feasible for the field. The testing reservoir was a sand-reservoir of a Klinkenberg permeability of 1.279 mD [11].

Zaitoun and Kohler (1988) [12] reported a set of experiments, in which at higher permeability ranges retention does no longer change. Furthermore, Vela *et al.* (1976) [13] showed that there is a significant decrease in retention when the permeability is increased from 12 mD to 137 mD. Permeability appears to be an important characteristic at the pore-scale and microscale level at values lower than 100 mD and becomes less important at higher permeabilities. Further results are summarized in Table 1 and serve for comparison purposes of the values calculated in this paper.

## 3. Fluids Optimization and Concentrations Selection

Two polymers in five different concentrations are tested during this work. Two Scleroglucan solutions and three Flopaam solutions. Different target viscosities were expected to be achieved in order to make the comparison more accurate. The fluids ought to be comparable and are therefore matched at their viscosity at a shear rate of  $25 \text{ s}^{-1}$ . The approach adopted for the comparison purpose is presented in Table 2. Fluids are tested before tracer particles and fluorescein sodium salt are added via Kinexus Pro rheometer at  $22^\circ\text{C}$  with a start shear of  $0.01 \text{ s}^{-1}$ , a final shear of  $5000.0 \text{ s}^{-1}$  and 10 samples per decade.

The preparation for both the brine and the polymer solutions (without induced mechanical degradation, non-sheared) is performed using the approach as utilized by Hincapie and Ganzer (2015) [6], Elhajjaji *et al.* (2016) [20] and Hincapie (2016) [21]. For the experiments in this work Synthetic Sea Water-Brine (SSW) was used for all solutions.

To be able to visualize the colorless polymer and brine flood through the micromodel, powder form of Fluorescein sodium salt by Sigma-Aldrich was added at 0.02% w/w concentration. Thus, enhancing the ability to follow the path the fluids are taking, as well as enabling plugging visibility under the UV-Light. One brine solution and all the polymer solutions were then mingled with 0.08% Sigma-Aldrich micro particles based on polystyrene with a size of  $1 \mu\text{m}$ . The fluorescein sodium salt sticks to the tracer particles, thereby coloring them and making them more visible on the photographs. In the initial experiment a lower percentage of tracer was tested, but did not make the plugging visible. Utilization of Fluorescein sodium salt was a proven approach presented by Födisch

**Table 1.** Summary of polymer retention experiments.

Polymer Type	Concentration [ppm]	Porous Media	Permeability [mD]	RF	RRF	Reference
HPAM		Glass Beads	3.98 - 4.55	360	3	[14]
Xanthan		Glass Beads	3.98 - 4.55	440	6	[14]
HPAM	500	Sandstone	1.279	-	3	[11]
HPAM	1000	-	-	1.68	1.47	[15]
HPAM	100	Quartz-Sand	-	13 - 16.1	3.5 - 4.9	[16]
Alcoflood (254S)	5000	Sand-Pack	-	4.47 - 6.04	1.17 - 1.54	[17]
Alcoflood (955)	20,000	Sand-Pack	-	5.13 - 6.1	1.45 - 2.03	[14]
HPAM	1500	Sand-Pack	2500 - 23,000	-	1 - 1.9	[18]
Xanthan	500 - 1000	Berea Plug	-	-	6	[19]

**Table 2.** Summary of polymers characteristics based on the evaluation approach.

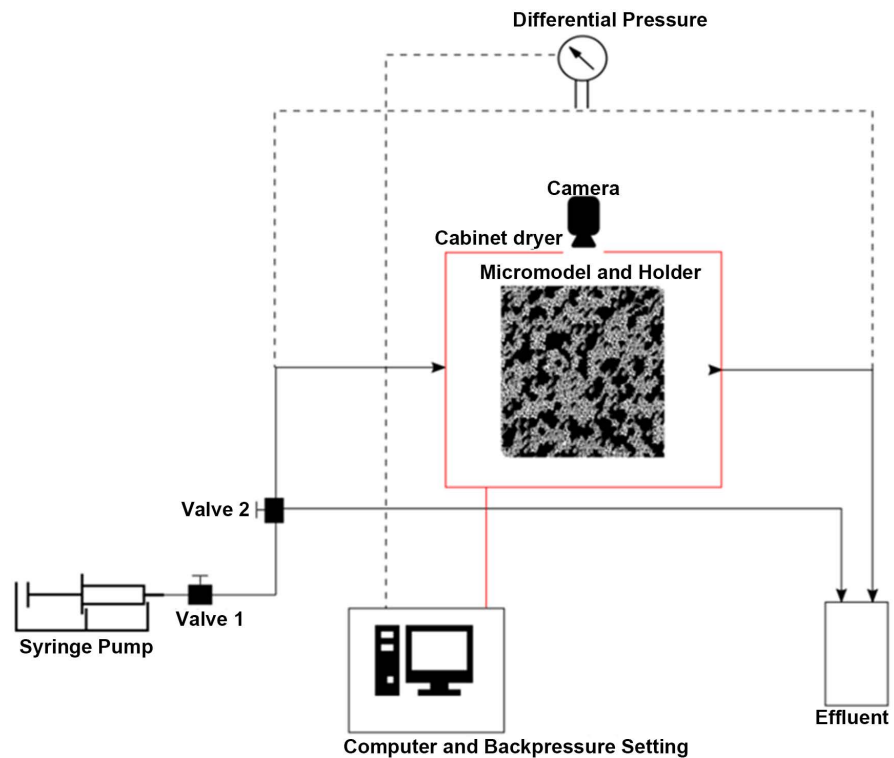
Desired Shear-Viscosity at Shear rate 25 s <sup>-1</sup> [mPas]	Scleroglucan (Biopolymer)			HPAM, Flopaam		
	Shear-Viscosity [mPas]	Shear-Viscosity with additives [mPas]	Concentration [ppm]	Shear-Viscosity [mPas]	Shear-Viscosity with additives [mPas]	Concentration [ppm]
~5	-	-		5.027	4.647	700
~10	-	-		8.307	7.501	1000
~15	12.99	12.82	600	17.8	17.5	1500
~25	24.42	24.26	1000	-	-	-

*et al.* (2015) [22]. The reason that only one out of two brine solutions are prepared with tracer particles is described more clearly in the methodology section. The first two steps in each experiment are to show that there is basically no influence of the tracer on the differential pressure, therefore we can conclude that the tracer particles themselves do not cause plugging. Furthermore, to describe the influence of these two additions to the polymer fluid, each solution is tested in the rheometer previous and after they are added.

#### 4. Micromodel and Setup

The experimental setup used in this work was specifically designed for micro-model EOR flooding experiments. The setup has proven to be very exact and to deliver reproducible results in the past for polymers and surfactants among others. The entire setup is placed in a darkroom with the reason being that the camera is very sensitive to light. Thus, the photographs could bleach at the slightest bit of brightness. The experimental setup consists of the following components depicted in **Figure 2** below:

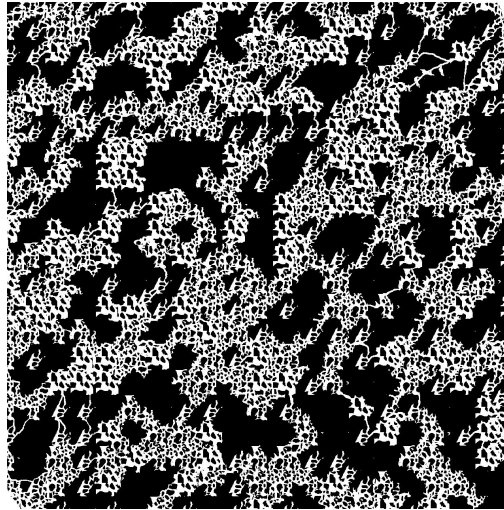
- Syringe pumps for fluid injection into the micromodel at the desired rate
- DLSR reflex camera



**Figure 2.** Schematic overview of the experimental setup used during this work.

- Pressure differential device to measure the pressure drop across the micro-model
- Valves and flow lines consisting of PTFE material and stainless steel
- A modified cabinet dryer with the camera and UV-Lights built in and able to heat the micromodel
- Back-pressure unit to install the pressure across the system accurately
- Glass Syringes with a capacity of 10 ml
- Computer connected to system to record photographs and differential pressure
- Micromodel Holder with an orange metal plate below it for better contrast

Micromodels have been used for several applications and evaluations, the flow behavior is addressed at the microscale by using microfluidics or lab-on-a-chip systems [23]-[28]. Micromodels used in this work are made of three layers, namely Glass-Silicon-Glass, and possess a size of 40 mm × 40 mm × 0.05 mm. To keep the micromodel transparent the porous structure is dry etched through the silicon. The silicon amidst two glass layers resembles a realistic, heterogeneous sandstone and is depicted in **Figure 3**. The arrows implicate the injection and production areas. The micromodel structure is derived from a  $\mu$ T image of a real unconsolidated sandstone or a thin-section, which is in the range of millimeters. An algorithm is used to create a large-scale image, whilst keeping the same properties, to create a micromodel utilizable for experiments, by adding patterns [29] [30] [31]. The characteristics of the used Micromodel can be seen



**Figure 3.** Binary image (lithographic mask) of the micromodel [29].

in **Table 3**. Permeability ( $k$ ) was measured during brine injection, at a rate of 2.5  $\mu\text{l}/\text{min}$ , according to Darcy and equals 1.14 D.

## 5. Experimental Methodology and Evaluation Methods

Prior the beginning of each experiment, it is important to ensure that the room and the cabinet have a temperature of about 22°C (room temperature). For correct differential pressure measurements is important to make sure that the pipelines and the micromodel are free of any air. If air should still be in the pipelines and the model, it has to be cleaned prior to starting the experiment. The back-pressure was initiated before every experiment and set to 3 bar. The experiments consist of six steps which are repeated with every polymer concentration. The differential pressure is recorded at every step of the experiment via software for qualitative analysis. A photograph is taken every minute for quantitative analysis.

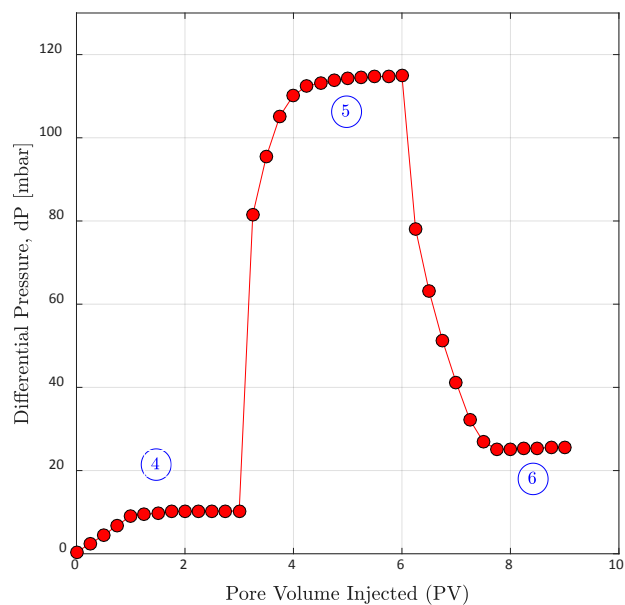
The workflow can be schematically understood and explained using **Figure 4**. Moreover, **Figure 5** describes in detail each step. An additional sequence for the workflow can be given as follows:

- Before injecting into the micromodel, 1 ml of the fluids is injected into the effluent container to fully saturate both sides.
- The first step of the experiment is to show the effect of the added tracer particles in aspect of plugging. To accomplish this, in the first step brine without tracer particles is injected at a rate of 2.5  $\mu\text{l}/\text{min}$  into the fully water saturated micromodel for about 40 minutes. This injection rate and length of injection will be the same for all the steps. At the first contact of the polymer fluid with the micromodel, 2 - 3 more pore volumes (PV) are injected. At a rate of 2.5  $\mu\text{l}/\text{min}$  each 10 minutes another PV is injected and the first contact was usually seen after  $\sim 10$  minutes.



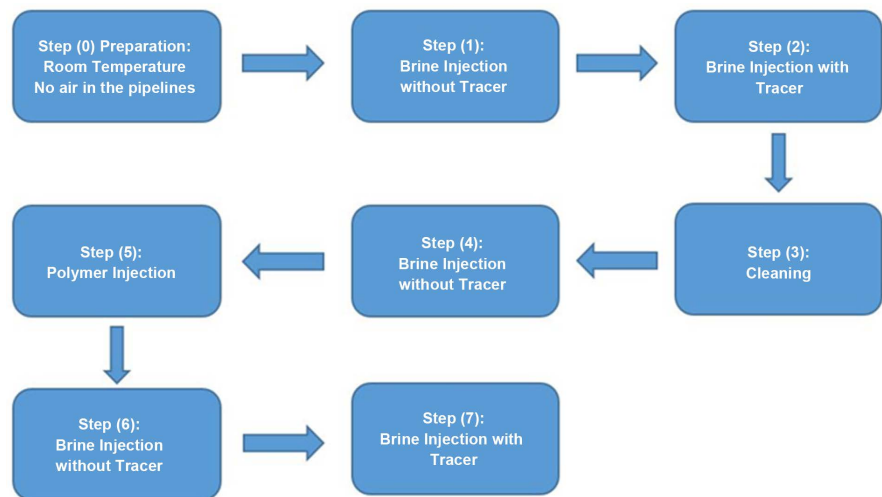
**Table 3.** Properties of the micromodel modified after Wegner (2015) [29], Herbas *et al.* (2015) [31] and Wegner *et al.* (2015) [32].

Property	Micromodel Value
Porosity [%]	34.07
Bulk volume (BV) [mm <sup>3</sup> ]	80
Pore volume (PV) [mm <sup>3</sup> ]	27.26
Average pore diameter [μm]	182.29
Min. pore diameter [μm]	62.60
Max. pore diameter [μm]	1682.10
Average grain size [mm <sup>2</sup> ]	0.31
Min. grain size [mm <sup>2</sup> ]	0.001
Max. grain size [mm <sup>2</sup> ]	57.09
Grain count [-]	3360
Specific-Surface [mm <sup>2</sup> /mm <sup>3</sup> ]	13.93
X-Tortuosity [-]	1.287
Y-Tortuosity [-]	1.189
Permeability	1.14 D

**Figure 4.** Schematic representation of the Experimental Steps as interpreted. Steps included here: Brine Injection without Tracer ④, Polymer Injection ⑤, Brine Injection without Tracer ⑥.

- During the second step, brine with added tracer particles is injected. It is will observed, that the differential pressure recorded during both stages depicted very similar or even identical behavior, thus leading to the result, that the tracer itself does not cause plugging.





**Figure 5.** Workflow of the steps undertaken to conduct experiments in this work.

- The third step is to clean the system. The tracer particles are not dissolvable, therefore have to be pushed out of the system. 4 ml Scleroglucan 600 - 800 ppm is injected at a rate of 500 µl/min. Afterwards 6 ml deionized water is injected at the same rate. This cleaning process is used during the experiments because it shows sufficient results. However, after each experiment the micromodel is cleaned more thorough with acid.
- In a fourth step, brine is injected without tracer to saturate the micromodel.
- Step 5 consists of the injection of the polymer with tracer, which is followed by another brine injection without tracer in step 6.
- Finally, brine with tracer is injected to be able to compare the results of step 2 and 7.

In matter of quantitative analysis, the reduction in permeability due to a variety of mechanisms can be calculated and represented as resistance factor (RF) and residual resistance factor (RRF). RF shows the enhancement of viscosity due to the polymer, also the mobility control capability, and RRF defines the permeability reduction in a porous medium due to retention [21].

$$RF = \frac{\Delta P(\text{Polymer})}{\Delta P(\text{Brine before Polymer Injection})} \quad (1)$$

$$RRF = \frac{\Delta P(\text{Brine after Polymer Injection})}{\Delta P(\text{Brine before Polymer Injection})} \quad (2)$$

Experiments with tracer particles are not able to visualize adsorption. This could be due to the fact that only retention mechanisms can be made visible where the tracer particles are stopped fully. Adsorption does narrow down even small passages, but does not usually block them, so that the tracer particles are still able to flow past. Thus, with adsorption not being made visible in the experiments the following equation is used to calculate the adsorption in a specific case.

$$\Gamma = (C_0 - C_e) \frac{V}{m} \quad (3)$$

where  $\Gamma$  [mg/g] is the polymer adsorption in porous media,  $C_0$  [ppm] is the initial polymer concentration,  $C_e$  [ppm] is the equilibrium polymer concentration,  $V$  [L] is the volume of the solution and  $m$  [g] is the weight of the adsorbent [2].

In matter of qualitative analysis, the photographs of the micromodel after the polymer injection are analyzed using a grid of  $10 \times 10$ . This helps defining the areas in which polymer retention occurred and is summarized in **Table 2**. The flowing part of the micromodel is calculated by:

$$\text{Flowing Grids} = \text{Overall Grids} - \text{Not Flowing Grids} \quad (4)$$

The grids, which showed polymer retention, in percentage from the overall flowing grids is then calculated by:

$$\text{Grids with visible retention} [\%] = \frac{\text{Grids with visible retention}}{\text{Flowing Grids}} * 100 \quad (5)$$

## 6. Qualitative Results

The qualitative analysis led to the assumption, that adsorption is not visible in the experiments conducted in this work. This will be further shown and proven in the quantitative analysis. Furthermore, only Flopaam showed a high amount of plugging throughout the entire micromodel. The values of plugged grids and flowing grids for each experiment are summarized in **Table 4**. The overall flow that the fluid establishes in the micromodel is depicted in **Figure 6**. The Grid-Images resulting after the polymer injection can be seen in **Figures 7-11**. The black grids resemble not-flowing grids of the micromodel, the yellow grids resemble zones in the micromodel, in which polymer retention was observed.

## 7. Quantitative Results

The RF and RRF for all experiments are depicted in **Figure 12** and **Figure 13** respectively, and summarized in **Table 3**. These values correspond nicely to the observations made earlier in this work. Scleroglucan solutions reached higher viscosity and therefore RF at lower concentrations. Furthermore, since adsorption seems to be the main mechanism of retention working during a biopolymer flood, the impact of it is displayed clearly. Scleroglucan 600 ppm reaches a lower RF than Flopaam 1500 ppm, but a higher RRF. Also, even though Flopaam 1500 ppm reaches the same RF value as Scleroglucan 1000 ppm, the RRF is reasonably lower.

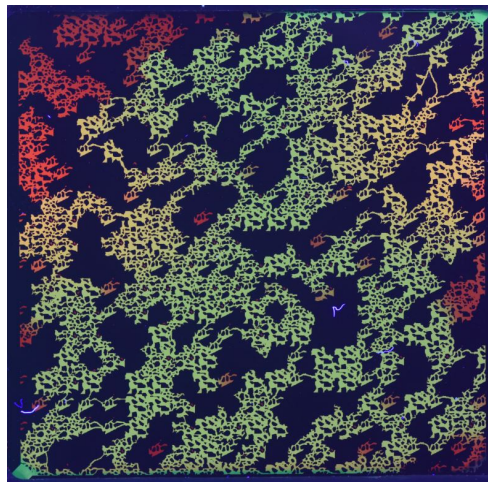
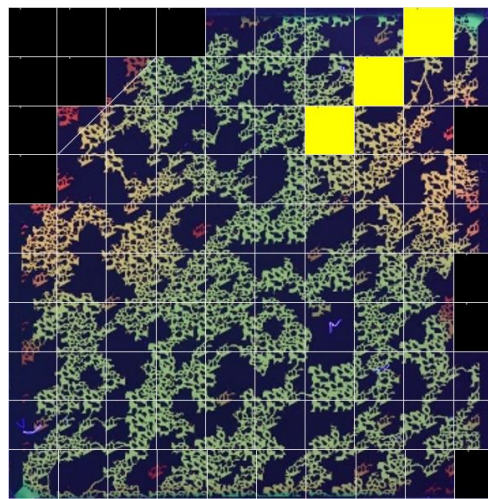
Flopaam reaches a higher RF in a concentration of 1000 ppm than with 700 ppm and therefore a higher viscosifying power, but the reduction in permeability is almost the same and almost neglectable. Flopaam 1000 ppm therefore seems to be very suitable for reservoirs similar to the micromodel used in this work. A concentration of 1500 ppm already shows a more significant reduction in permeability.

For the Scleroglucan 600 ppm the effluents were collected and tested and resulted in a viscosity of 11.68 mPas at a shear rate of  $25 \text{ s}^{-1}$ . The concentration and viscosity of further test results of Scleroglucan at shear-rate  $25 \text{ s}^{-1}$  were

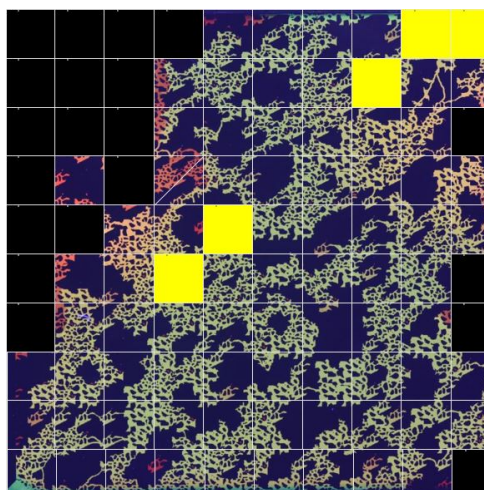
**Table 4.** Summary of the qualitative analysis.

Polymer	Concentration [ppm]	Flowing Grids [%]	Grids with visible retention* [%]	Visible Retention
BIO-Scleroglucan	600	87.0	3.45	Low
BIO-Scleroglucan	1000	79.5	6.29	Intermediate
HPAM-Flopaam	700	83.0	2.41	Low
HPAM-Flopaam	1000	86.5	5.78	Intermediate
HPAM-Flopaam	1500	87.0	19.54	High

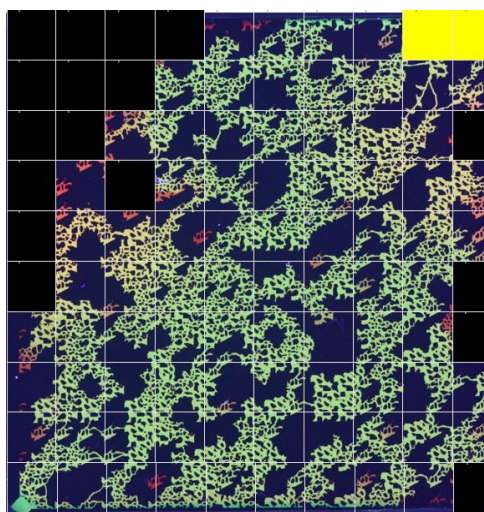
\*Percentage of the flowing grids.

**Figure 6.** Overall flow establishing in the micromodel.**Figure 7.** Grid image of scleroglucan 600 ppm.

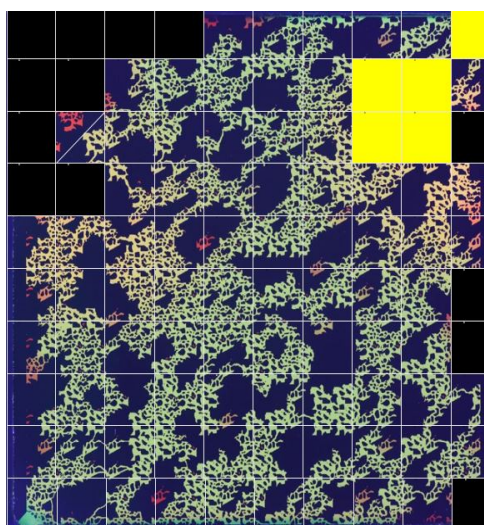
plotted in **Figure 14**, the equilibrium concentration could be determined and equals 536.52 ppm. The density of the silica is approximately  $2.23 \text{ g/cm}^3$ . The volume of the silica is calculated by subtracting the volume of the porosity from the total volume, Equation (6). The mass was then calculated via Equation (7) and the adsorption could be determined in Equation (8).



**Figure 8.** Grid image of scleroglucan 1000 ppm.

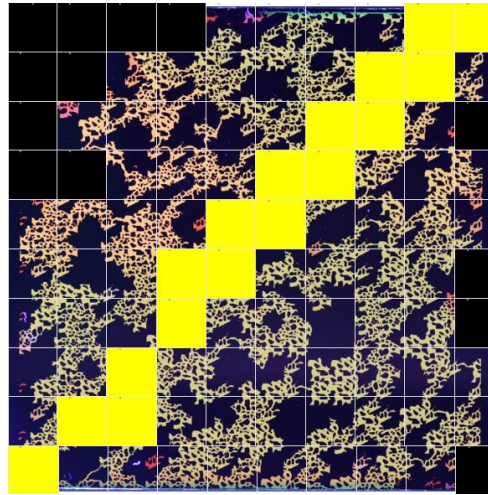


**Figure 9.** Grid image of flopaam 700 ppm.

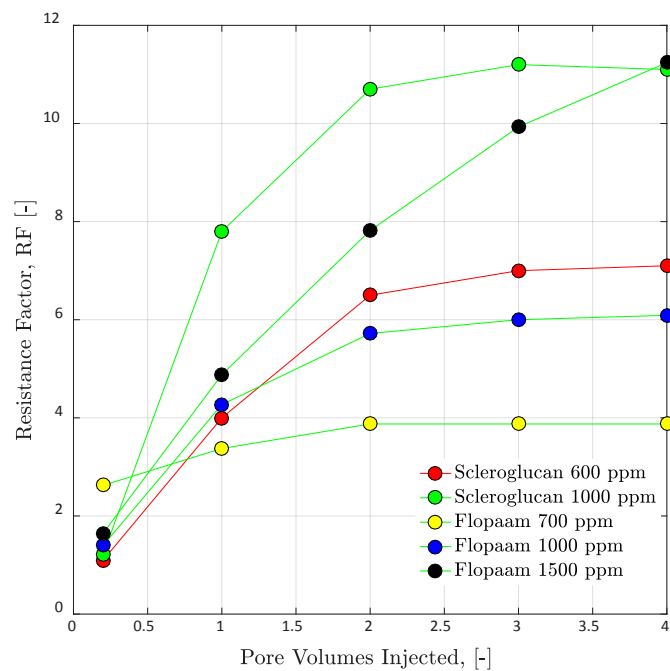


**Figure 10.** Grid image of flopaam 1000 ppm.





**Figure 11.** Grid image of flopaam 1500 ppm.



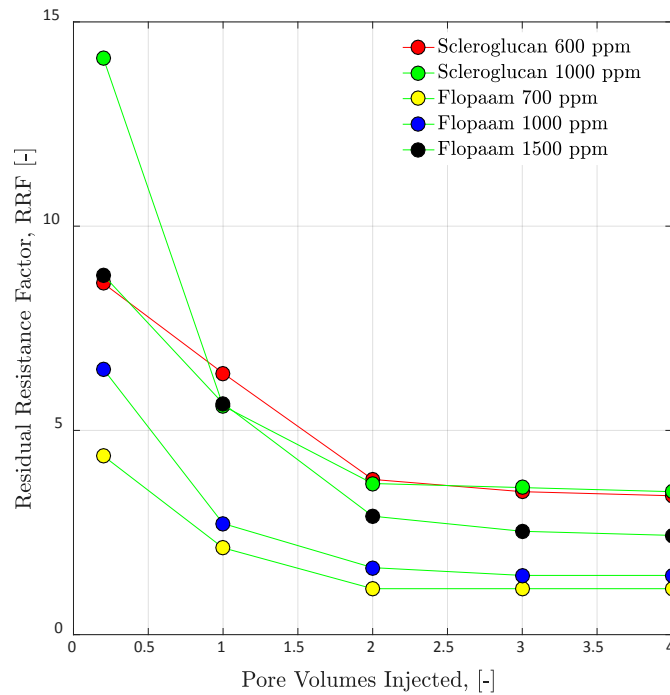
**Figure 12.** Summary of the resistance factor of all polymers.

$$V[\text{mm}^3](\text{silica}) = 80 \text{ mm}^3 - (80 \text{ mm}^3 * 0.3407) = 52.744 \quad (6)$$

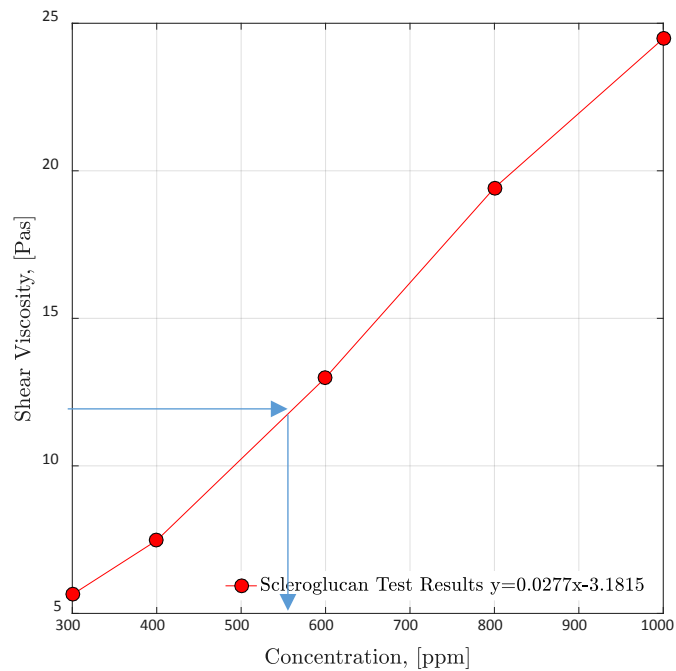
$$m[\text{g}](\text{silica}) = 0.00223 \left[ \frac{\text{g}}{\text{mm}^3} \right] * 52.744 [\text{mm}^3] = 0.1176 \quad (7)$$

$$\Gamma [\text{mg/g}] = (C_0 - C_e) \frac{V}{m} = (600 - 536.52) \frac{0.008}{0.1176} = 4.318 \quad (8)$$

This result equals 4318  $\mu\text{g/g}$  of adsorption and is a very high result comparing it to the values found in previous experiments. This value should be considered with caution, since the experiment was running for two days under room



**Figure 13.** Summary of the residual resistance factor of all polymers.



**Figure 14.** Scleroglucan viscometer results at shear-rate  $25 \text{ s}^{-1}$ .

temperature. Uncertainties, such as the degradation of the polymer are not included. Nevertheless, it implies a very large amount of adsorption for the biopolymer.

All in all, it can be seen in the data, that the adsorption in biopolymers is a large issue for polymer flooding in media with low permeability (Table 5).

**Table 5.** Summary of the quantitative results obtained.

Polymer	Concentration [ppm]	Shear-Viscosity at 25 s <sup>-1</sup> with additives [mPas]	Resistance Factor [-]	Residual Resistance Factor [-]
Flopaam 6035 S	700	4.647	3.881	1.039
	1000	7.500	5.722	1.386
	1500	17.500	11.278	2.446
Scleroglucan	600	12.820	6.893	3.327
	1000	24.260	10.946	3.450

## 8. Summary and Conclusions

In this work, polymer flooding experiments have been successfully conducted. The polymers varied in type and concentration. Tracer particles in combination with fluorescein sodium salt helped to visualize polymer flow through the Glass-Silicon-Glass micromodel, resembling a low permeable reservoir. Images were taken during the flooding process and the results gave provided additional insights into the flow of polymers through such micromodels and into the retention mechanisms working principle.

According to our results, the main retention mechanism in Flopaam flooding experiments was mechanical entrapment, whereas Scleroglucan flooding experiments were adsorption. The quantitative analysis provided the information that adsorption is not visible in this kind of experiments. Also, the Scleroglucan resulted in a higher RRF in both experiments, even though a Flopaam with a higher RF was tested. Furthermore, an increase in concentration led to a rise in RF for both Polymers and RRF for the HPAM. The qualitative analysis provided that most polymer solutions showed a filtration-like process at the injection side. Also, while Flopaam 1000 ppm showed almost no visible plugging, the visible plugging for a concentration of 1500 ppm increased sharply. There seems to be a critical concentration for Flopaam, at which there is a steep rise in permeability reduction. On the other hand, Scleroglucan seems to establish the same amount of adsorption in low concentrations. Adsorption has a larger influence on the RRF than mechanical entrapment. At such low flow-rates, none of the polymers used showed hydrodynamic retention. Moreover, we demonstrated that the workflow presented in this work can be utilized to assess any kind of fluid in order to determine the potential effects in permeability reductions or plugging.

## Acknowledgements

The authors are thankful to the Institute of Petroleum Engineering (ITE) from Clausthal University of Technology in Germany, for providing the necessary facilities and financial support for the investigation. The authors also acknowledge the support given by the Open Access Publishing Fund of Clausthal University of Technology.



## References

- [1] Hincapie, R., Tovar, F.D. and Alvarez, C.E. (2011) Feasibility for the Application of In Situ Combustion in Faja Petrolifera del Orinoco (FPO) Based in a Novel Screening Criteria for the Technology. Society of Petroleum Engineers, Kuala Lumpur.
- [2] Sorbie, K. (1990) Polymer-Improved Oil Recovery. CRC Press Inc., Boca Raton, 126-164.
- [3] Hincapie, R.E., Alvarez, C.E. and Vargas, A.J. (2011) Technical Feasibility of Polymer Injection in Heavy Oil Reservoir BAINF60 and BAMED78: Intercampo Norte—Through Predictive Models. *SPE Heavy Oil Conference and Exhibition*, Kuwait City, 12-14 December 2011, SPE-149621-MS.
- [4] Mezger, T.G. (2011) The Rheology Handbook. 3rd Edition, Vincentz Network GmbH & Co KG, Hanover.
- [5] Seright, R.S., Seheult, J.M. and Talashek, T. (2009) Injectivity Characteristics of EOR Polymers. *SPE Annual Technical Conference and Exhibition*, Denver, Colorado, 21-24 September 2009, SPE-115142-MS. <https://doi.org/10.2118/115142-PA>
- [6] Hincapie, R.E. and Ganzer, L. (2015) Assessment of Polymer Injectivity with Regards to Viscoelasticity: Lab Evaluations towards Better Field Operations. *EUROPEC 2015*, Madrid, 1-4 June 2015, SPE-174346-MS.
- [7] Sheng, J.J. (2010) Modern Chemical Enhanced Oil Recovery—Theory and Practice. Elsevier, Amsterdam.
- [8] Thomas, A. (2016) Polymer Flooding. InTech. <https://doi.org/10.5772/64623>
- [9] Manichand, R. and Seright, R.S. (2014) Field vs. Laboratory Polymer-Retention Values for a Polymer Flood in the Tambaredjo Field. *SPE Improved Oil Recovery Symposium*, Tulsa, 12-16 April 2014, SPE-169027-MS.
- [10] Yerramilli, S., Zitha, P. and Yerramilli, C. (2013) Novel Insight into Polymer Injectivity for Polymer Flooding. *SPE European Formation Damage Conference & Exhibition*, Noordwijk, 5-7 June 2013, SPE-165195-MS.
- [11] Castro-Garcia, R.H., Maya-Toro, G., Jimenes-Diaz, R., Quintero-Perez, H., Diaz-Guardia, V., Colmenares-Vargas, K., Palma-Bustamante, J., Delgadillo-Aya, C. and Perez-Romero, R. (2016) Polymer Flooding to Improve Volumetric Sweep Efficiency in Waterflooding Processes. CT&F—Ciencia, Tecnologia y Futuro, Santander, Columbia.
- [12] Zaitoun, A. and Kohler, N. (1988) Two-Phase Flow through Porous Media: Effect of an Adsorbed Polymer Layer. Society of Petroleum Engineers, Houston.
- [13] Vela, S., Peaceman, D. and Sandvik, E. (1976) Evaluation of Polymer Flooding in a Layered Reservoir with Crossflow, Retention and Degradation. *SPE J*, **16**, 82-96. <https://doi.org/10.2118/5102-PA>
- [14] Wei, B., Romero-Zerón, L. and Rodrigue, D. (2013) Mechanical Properties and Flow Behaviour of Polymers for Enhanced Oil Recovery. Taylor & Francis, Abingdon-on-Thames.
- [15] De Melo, M.A., de Holleben, C.R.C., da Silva, I.P.G., de Barros Correia, A., da Silva, G.A., Rosa, A.J., Lins, A.G. and de Lima, J.C. (2005) Evaluation of Polymer-Injection Projects in Brazil. Society of Petroleum Engineers, Rio de Janeiro.
- [16] Lu, X., Liu, H., Wang, S. and Wang, X. (2011) Performance Evaluation and Mechanism Analysis of HPAM Solutin with Broad-Distribution Relative Molecular Mass. *International Petroleum Technology Conference*, Bangkok, 15-17 November 2011, 12. <https://doi.org/10.2523/IPTC-14352-MS>

- [17] Tu, T.N. and Bae, W. (2011) Investigating the Effect of Polymer Gels Swelling Phenomenon under Reservoir Conditions on Polymer Conformance Control Process. *International Petroleum Technology Conference*, Bangkok, 15-17 November 2011, 11. <https://doi.org/10.2523/IPTC-14673-MS>
- [18] Wassmuth, F.R., Green, K. and Bai, J. (2012) Associative Polymers Outperform Regular Polymers Displacing Heavy Oil in Heterogeneous Systems. Society of Petroleum Engineers, Calgary. <https://doi.org/10.2118/157916-MS>
- [19] Fletcher, A., Flew, S.R.G., Lamb, S.P., Lund, T., Bjornestad, E., Stavland, A. and Gjovikli, N.B. (1991) Measurements of Polysaccharide Polymer Properties in Porous Media. Society of Petroleum Engineers, Anaheim.
- [20] Elhajjaji, R.R., Hincapie, R.E., Tahir, M., Rock, A., Wegner, J. and Ganzer, L. (2016) Systematic Study of Viscoelastic Properties during Polymer-Surfactant Flooding in Porous Media. Society of Petroleum Engineers, Moscow. <https://doi.org/10.2118/181916-MS>
- [21] Hincapie, R.E. (2016) Pore-Scale Investigation of the Viscoelastic Phenomenon during Enhanced Oil Recovery (EOR) Polymer Flooding through Porous Media. Papierflieger Verlag GmbH, Clausthal-Zellerfeld.
- [22] Foedisch, H., Wegner, J., Hincapie, R.E. and Ganzer, L. (2015) Impact of Connate Water Replacement on Chemical EOR Processes. Society of Petroleum Engineers, Quito. <https://doi.org/10.2118/177196-MS>
- [23] Clarke, A., Howe, A.M., Mitchell, J., Staniland, J. and Hawkes, L.A. (2016) How Viscoelastic Polymer Flooding Enhances Displacement Efficiency. Society of Petroleum Engineers, Quito.
- [24] Galindo-Rosales, F.J., Campo-Deaño, L., Pinho, F.T., van Bokhorst, E., Hamersma, P.J., Oliveira, M.S.N. and Alves, M.A. (2011) Microfluidic Systems for the Analysis of Viscoelastic Fluid Flow Phenomena in Porous Media. *Microfluidics and Nanofluidics*, **12**, 485-498. <https://doi.org/10.1007/s10404-011-0890-6>
- [25] Hincapie, R.E., Rock, A., Wegner, J. and Ganzer, L. (2017) Oil Mobilization by Viscoelastic Flow Instabilities Effects during Polymer EOR: A Pore-Scale Visualization Approach. Society of Petroleum Engineers, Buenos Aires.
- [26] Rock, A., Hincapie, R.E., Wegner, J. and Ganzer, L. (2017) Advanced Flow Behavior Characterization of Enhanced Oil Recovery Polymers. Society of Petroleum Engineers, Paris.
- [27] Be, M., Hincapie, R.E., Rock, A., Gaol, C.L., Tahir, M. and Ganzer, L. (2017) Comprehensive Evaluation of the EOR Polymer Viscoelastic Phenomenon at Low Reynolds Number. Society of Petroleum Engineers, Paris.
- [28] Rock, A., Hincapie, R.E., Wegner, J., Foedisch, H. and Ganzer, L. (2017) Pore-Scale Visualization of Oil Recovery by Viscoelastic Flow Instabilities during Polymer EOR. European Association of Geoscientists and Engineers, Stavanger. <https://doi.org/10.3997/2214-4609.201700273>
- [29] Wegner, J. (2015) Investigation of Polymer Enhanced Oil Recovery (EOR) in Microfluidic Devices that resemble Porous Media—An Experimental and Numerical Approach. Institute of Petroleum Engineering, Clausthal-Zellerfeld.
- [30] Foedisch, H., Hincapie, R., Wegner, J. and Ganzer, L. (2015) Visualization of Connate Water Replacement during Flooding Experiments Using Glass-Silicon-Glass Micromodels. *First Break Magazine*.
- [31] Herbas, J.G., Wegner, J., Hincapie, R.E., Foedisch, H., Ganzer, L., Castillo, J.A.D. and Mugizi, H.M. (2015) Comprehensive Micromodel Study to Evaluate Polymer EOR in Unconsolidated Sand Reservoirs. Society of Petroleum Engineers, Manama.

<https://doi.org/10.2118/172669-MS>

- [32] Wegner, J., Hincapie, R.E., Foedisch, H. and Ganzer, L. (2015) Novel Visualisation of Chemical EOR Flooding Using a Lab-on-a-Chip Setup Supported by an Extensive Rheological Characterisation. Society of Petroleum Engineers, Kuala Lumpur.
- <https://doi.org/10.2118/174648-MS>